

## Homework 2 Solutions

Problems for Chapter 2

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Section 2-1

2-1. Derive Eqs. (2-5).

We follow the procedure used to derive Eq. (2-4) (see Fig. 2-2 where the values of stress components are properly modified).

FACE	MOMENT ABOUT y-AXIS
BCGF	$(\sigma_{xx} + d\sigma_{xx}) dy dz \frac{dx}{2} - (\sigma_{xx} + d\sigma_{xx}) dy dz dx$
CDHG	$-(\sigma_{yx} + d\sigma_{yx}) \frac{dx}{2} dx dz + (\sigma_{yx} + d\sigma_{yx}) \frac{dx}{2} dx dz$
ADHE	$-\sigma_{xx} \frac{dx}{2} dy dz$
AEFB	$\sigma_{yx} \frac{dx}{2} dx dz - \sigma_{yx} \frac{dx}{2} dx dz$
ABCD	$\sigma_{xx} \frac{dx}{2} dx dy$
FGHE	$-(\sigma_{xx} + d\sigma_{xx}) \frac{dx}{2} dx dy + (\sigma_{xx} + d\sigma_{xx}) dz dx dy$

Summing up these expressions and adding moments due to the body forces we obtain:

$$\begin{aligned}
 & (\sigma_{xx} + d\sigma_{xx}) dz dy \frac{dx}{2} - (\sigma_{xx} + d\sigma_{xx}) dx dy dz - (\sigma_{yx} + d\sigma_{yx}) \frac{dx}{2} dx dz \\
 & + (\sigma_{yx} + d\sigma_{yx}) \frac{dx}{2} dx dz - \sigma_{xx} \frac{dx}{2} dx dz + \sigma_{yx} \frac{dx}{2} dx dz - \sigma_{yx} \frac{dx}{2} dx dz \\
 & + \sigma_{xx} \frac{dx}{2} dx dy - (\sigma_{xx} + d\sigma_{xx}) \frac{dx}{2} dx dy + (\sigma_{xx} + d\sigma_{xx}) dz dx dy \\
 & + b_x dx dy dz \frac{dx}{2} - b_x dx dy dz \frac{dx}{2}.
 \end{aligned}$$

Next we substitute these expressions into Eq (2-3):

$$\sum M_y = 0.$$

On discarding smaller order terms and dividing this equation through by  $dx dy dz$  we get

$$\sigma_{xz} = \sigma_{zx} \quad (2-5)$$

Similarly

FACE	MOMENT ABOUT z-AXIS
BCGF	$-(\sigma_{xz} + d\sigma_{xz}) \underset{\text{stress}}{dy dz} \underset{\text{area}}{\frac{dx}{2}} + (\sigma_{yz} + d\sigma_{yz}) \underset{\text{moment arm}}{dx dz}$
CDHG	$(\sigma_{yz} + d\sigma_{yz}) \frac{dx}{2} dx dz - (\sigma_{xz} + d\sigma_{xz}) dy dx dz$
ADHE	$\sigma_{xz} \frac{dy}{2} dy dz$
AEFB	$-\sigma_{yz} \frac{dx}{2} dx dz$
ABCD	$\sigma_{xz} \frac{dy}{2} dx dy - \sigma_{yz} \frac{dx}{2} dx dy$
FGHE	$-(\sigma_{xz} + d\sigma_{xz}) \frac{dy}{2} dx dy + (\sigma_{yz} + d\sigma_{yz}) \frac{dx}{2} dx dy$

Summing up these expressions and adding moments due to the body forces we obtain:

$$\begin{aligned}
& -(\sigma_{xx} + d\sigma_{xx})dz dy \frac{dy}{2} + (\sigma_{xx} + d\sigma_{xx})dx dy dz \\
& + (\sigma_{yy} + d\sigma_{yy})\frac{dx}{2} dx dz - (\sigma_{yy} + d\sigma_{yy})dy dx dz \\
& + \sigma_{xx} \frac{dy}{2} dy dz - \sigma_{yy} \frac{dx}{2} dx dz + \sigma_{zz} \frac{dy}{2} dx dy - \sigma_{zz} \frac{dx}{2} dx dy \\
& - (\sigma_{xx} + d\sigma_{xx})\frac{dy}{2} dx dy + (\sigma_{yy} + d\sigma_{yy})\frac{dx}{2} dx dy \\
& - b_x dx dy dz \frac{dy}{2} + b_y dx dy dz \frac{dx}{2}.
\end{aligned}$$

Next we substitute these expressions into Eq.(2-3):

$$\sum M_z = 0.$$

On discarding smaller order terms and dividing this equation through by  $dx dy dz$  we get

$$\sigma_{xy} = \sigma_{yx} \quad (2-5)$$

2-2. Show all steps in the derivation of Eq (2-13).  
Substituting Eq.(2-8) into Eq.(2-12) we get

$$t^{(n)} \Delta A + t^{(-x)} n_x \Delta A + t^{(-y)} n_y \Delta A + t^{(-z)} n_z \Delta A + \frac{h}{2} \Delta A b = 0$$

In the limit, with  $h \rightarrow 0$  and taking into account that  $t^{(-y)} = -t^{(y)}$  etc, we find that:

$$t^{(n)} = t^{(x)} n_x + t^{(y)} n_y + t^{(z)} n_z \quad (2-13)$$

2-3. Derive Eq.(2-17), then write it as a product of three matrices.

Substituting Eq.(2-7) into Eq.(2-16) we get

$$\begin{aligned}
\sigma_n = & [t^{(x)} \cdot (n_x i + n_y j + n_z k)] n_x + [t^{(y)} \cdot (n_x i + n_y j + n_z k) t^{(x)}] n_y + \\
& + [t^{(z)} \cdot (n_x i + n_y j + n_z k)] n_z
\end{aligned}$$

Using Eq.(2-1) to replace the dot products leads to

... with the equation (2-30) which when multiplied by  $\mathbf{i}$  gives

$$\mathbf{s} \cdot \mathbf{i} = (t^{(x)} \cdot \mathbf{i} n_x + t^{(y)} \cdot \mathbf{i} n_y + t^{(z)} \cdot \mathbf{i} n_z - \sigma_n \mathbf{n} \cdot \mathbf{i}) / \tau$$

Using here Eq.(2-1) and Eq.(2-7) we get the first of Eqs.(2-31)

$$s_x = (\sigma_{xx} n_x + \sigma_{xy} n_y + \sigma_{xz} n_z - \sigma_n n_x) \tau,$$

The other two are obtained in the same way.

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2-7. The stress matrix  $\mathbf{S}$  at a point  $M$  is given by

$$\mathbf{S} = \begin{bmatrix} 2 & 1 & 2 \\ 1 & 3 & 0 \\ 2 & 0 & 2 \end{bmatrix}$$

Draw a plane  $T$  through  $M$  with the direction cosines:

$$n_x = \frac{1}{\sqrt{3}}, \quad n_y = \frac{1}{\sqrt{3}}, \quad n_z = \frac{1}{\sqrt{3}}.$$

Find:

- (a) the traction vector  $\mathbf{t}^{(n)}$  acting on  $T$  at  $M$ ,  
 (b) its Cartesian components  $t_x^{(n)}$ ,  $t_y^{(n)}$ , and  $t_z^{(n)}$   
 (c) its normal component  $\sigma_n$ .

We follow the procedure outlined in Example 2-4.

- (a) First we identify the stress components from the matrix  $S$ :  $s_{xx}=2$ ,  $s_{yy}=1$ ,  $s_{zz}=2$ ,  $s_{xy}=3$ ,  
 $s_{yz}=0$ ,  $s_{zx}=2$ . Next we evaluate the traction vector acting at  $M$ :

$$\mathbf{t}^{(n)} = t_x^{(n)} \mathbf{i} + t_y^{(n)} \mathbf{j} + t_z^{(n)} \mathbf{k}$$

where the components of  $\mathbf{t}^{(n)}$  are given by (Eq.2-14). Thus

$$\mathbf{t}^{(n)} = (\sigma_{xx}n_x + \sigma_{xy}n_y + \sigma_{xz}n_z) \mathbf{i} + (\sigma_{xy}n_x + \sigma_{yy}n_y + \sigma_{yz}n_z) \mathbf{j} \\ + (\sigma_{xz}n_x + \sigma_{yz}n_y + \sigma_{zz}n_z) \mathbf{j}$$

and finally, substituting the numerical values for the stress components and direction cosines we get

$$\mathbf{t}^{(n)} = (5\mathbf{i} + 4\mathbf{j} + 4\mathbf{k}) / \sqrt{3}$$

(b) Now:

$$t_x^{(n)} = (2 + 1 + 2) / \sqrt{3} = 5 / \sqrt{3}, t_y^{(n)} = (1 + 3 + 0) / \sqrt{3} = 4 / \sqrt{3},$$

$$t_z^{(n)} = (2 + 0 + 2) / \sqrt{3} = 4 / \sqrt{3}$$

(c) Substituting the data into Eq.(2-17) we get

$$\sigma_n = (2 + 3 + 2 + 2 \cdot 1 + 2 \cdot 2 + 2 \cdot 0) \cdot \frac{1}{3} = 13/3$$

2-8. A solid, rectangular bar is subject to uniform tension  $q$  per unit area (Fig.P2-8). The state of stress inside the bar was found to be also uniform such that  $\sigma_{xx} = q$ , and all other stress components equal to zero. Find the normal component  $\sigma_n$ , and the tangential component  $\tau$ , of the traction  $\mathbf{t}^{(n)}$  acting at an inside point on the plane with the outer normal

$x_1 = 35 - 25 = 10$  (normal stress)  
 $x_2 = 35 - 35 = 0$  (normal stress)  
 $x_3 = 35 - 35 = 0$  (normal stress)

$\sigma_x = 10$  (normal stress)  
 $\sigma_y = 0$  (normal stress)  
 $\sigma_z = 0$  (normal stress)

$\tau_{xy} = 0$   
 $\tau_{yz} = 0$   
 $\tau_{zx} = 0$

$\sigma_x = 10$   
 $\sigma_y = 0$   
 $\sigma_z = 0$   
 $\tau_{xy} = 0$   
 $\tau_{yz} = 0$   
 $\tau_{zx} = 0$



$$N = i + 2j + k$$

Hint:

$$n = \frac{N}{|N|}$$

We have

$$n = (i + 2j + k) / \sqrt{1 + 4 + 1} = (i + 2j + k) / \sqrt{6}$$

Hence:  $n_x = 1/\sqrt{6}$ ,  $n_y = 2/\sqrt{6}$ ,  $n_z = 1/\sqrt{6}$

Using Eq.(2-17) where we substitute the known values of stress components we get:  $s_n = q/6$ .

Finally, from Eq.(2-27) we obtain

$$\tau = \sqrt{q^2/6 - q^2/36} = \frac{\sqrt{5}}{6}q$$