

MECH 5312 – Solid Mechanics II

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Principal Strains

- **Principal stresses** exists on an Arbitrary plane, \mathbf{n} in a body where only normal stresses appear. Find two complementary planes that are orthogonal to \mathbf{n} . We arrive at the **principal stress tensor**.

$$\boldsymbol{\sigma} = \begin{array}{ccc} & \mathbf{n}_1 & \mathbf{n}_2 & \mathbf{n}_3 \\ \left[\begin{array}{ccc} \sigma_1 & 0 & 0 \\ 0 & \sigma_2 & 0 \\ 0 & 0 & \sigma_3 \end{array} \right] & \mathbf{n}_1 & \mathbf{n}_2 & \mathbf{n}_3 \end{array}$$

- What form does the corresponding **principal strain tensor** take?

Principal Strain Tensor

- Since, the **principal stress tensor** contains **only normal stresses**, the **principal strain tensor** will contain **only normal strains**.

$$\boldsymbol{\varepsilon} = \begin{array}{ccc} & \mathbf{n}_1 & \mathbf{n}_2 & \mathbf{n}_3 \\ \left[\begin{array}{ccc} \boldsymbol{\varepsilon}_1 & 0 & 0 \\ 0 & \boldsymbol{\varepsilon}_2 & 0 \\ 0 & 0 & \boldsymbol{\varepsilon}_3 \end{array} \right] & \mathbf{n}_1 & \mathbf{n}_2 & \mathbf{n}_3 \end{array}$$

- Our procedure for finding the principal strains follows

Principal Strain

- The principal directions coincide with Arbitrary plane, \mathbf{n} through the body where the normal strain, ε_n is maximized and shear strain disappears, $\gamma = 0$

$$\begin{bmatrix} (\varepsilon_{xx} - \varepsilon_n) & \varepsilon_{xy} & \varepsilon_{xz} \\ \varepsilon_{yx} & (\varepsilon_{yy} - \varepsilon_n) & \varepsilon_{yz} \\ \varepsilon_{zx} & \varepsilon_{zy} & (\varepsilon_{zz} - \varepsilon_n) \end{bmatrix} \begin{bmatrix} n_x \\ n_y \\ n_z \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix}$$

$$(\boldsymbol{\varepsilon} - \varepsilon_n \mathbf{I}) \mathbf{n} = \mathbf{0}$$

$$\sqrt{n_x^2 + n_y^2 + n_z^2} = 1$$

Strain Invariants

- The exact solution to the determinant

$$\det(\boldsymbol{\varepsilon} - \varepsilon_n \mathbf{I}) = 0$$

- resolves into a quadratic equation

$$\varepsilon_n^3 - J_1 \varepsilon_n^2 + J_2 \varepsilon_n - J_3 = 0$$

- where J_1 , J_2 , and J_3 are the strain Invariants.

$$J_1 = \text{tr}(\boldsymbol{\varepsilon}) = \varepsilon_{xx} + \varepsilon_{yy} + \varepsilon_{zz}$$

$$J_2 = \varepsilon_{xx} \varepsilon_{yy} + \varepsilon_{yy} \varepsilon_{zz} + \varepsilon_{zz} \varepsilon_{xx} - \varepsilon_{xy}^2 - \varepsilon_{xz}^2 - \varepsilon_{yz}^2$$

$$J_3 = \det(\boldsymbol{\varepsilon})$$

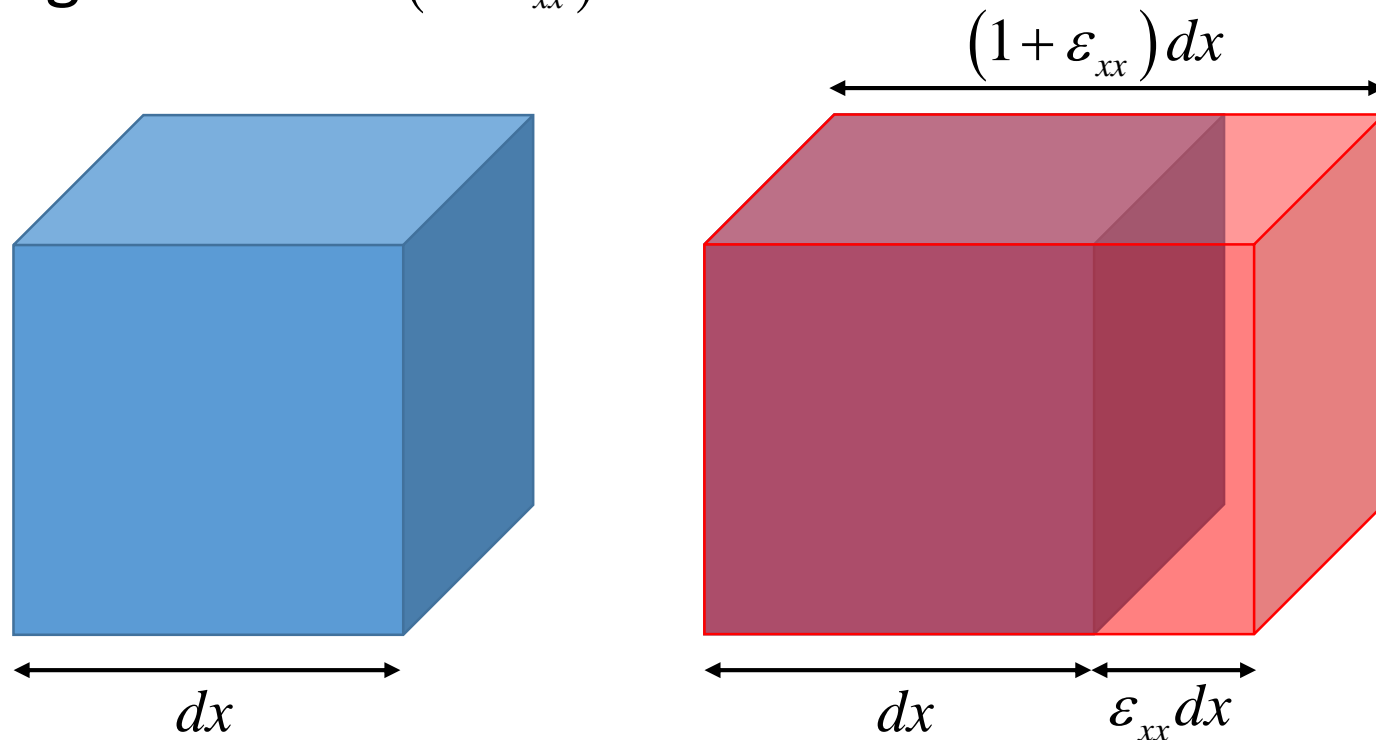
Example

MathCAD

Volume Change and Dilatation

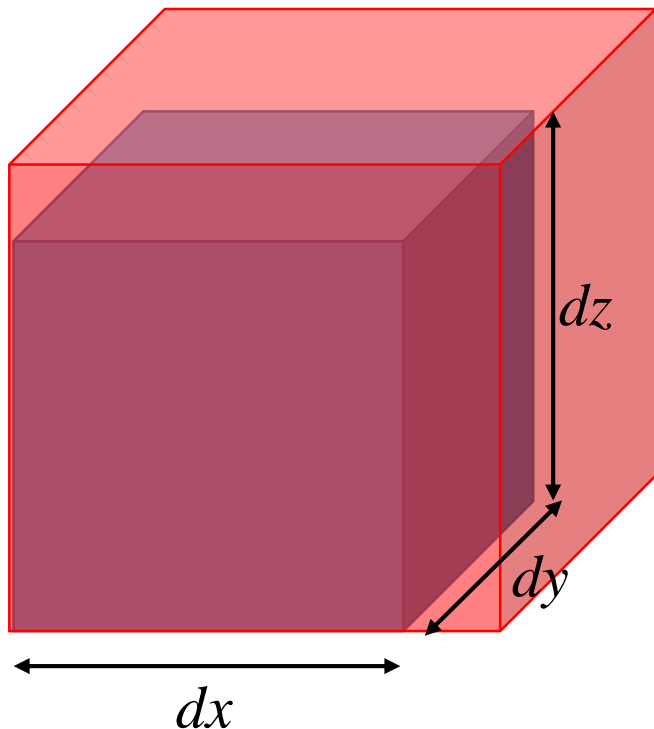
- A differential element is subject to normal strain ε_{xx} in the x direction
- The length of the side increases by $\varepsilon_{xx} dx$
- The new length is now $(1 + \varepsilon_{xx}) dx$

Example, for dx



Volume Change and Dilatation

- If the differential element is subject to normal strains ε_{xx} , ε_{yy} , ε_{zz}
- The lengths of the sides increase by $\varepsilon_{xx} dx$, $\varepsilon_{yy} dy$, $\varepsilon_{zz} dz$
- The new lengths are now $(1 + \varepsilon_{xx}) dx$, $(1 + \varepsilon_{yy}) dy$, $(1 + \varepsilon_{zz}) dz$



The Initial Volume, V

$$V = dx dy dz$$

The Deformed Volume, V_{def}

$$V_{def} = (1 + \varepsilon_{xx})(1 + \varepsilon_{yy})(1 + \varepsilon_{zz}) dx dy dz$$

Volume Change and Dilatation

- Assuming finite displacement, the change in volume becomes

$$\Delta V = V_{def} - V_0 = (\varepsilon_{xx} + \varepsilon_{yy} + \varepsilon_{zz}) dx dy dz$$

Second order terms are neglected!

- The change in volume per unit volume is

$$V = dx dy dz$$

$$\Delta \equiv \frac{\Delta V}{V} = \varepsilon_{xx} + \varepsilon_{yy} + \varepsilon_{zz}$$

- where Δ is the dilatation and

$$\Delta = J_1$$

Strain Deviator

- Strain can be decomposed into volumetric and deviatoric parts

$$\boldsymbol{\varepsilon} = \left(\frac{1}{3} \Delta \right) \mathbf{I} + \boldsymbol{\varepsilon}_d$$

- The deviatoric strain can be found by rearranging

$$\boldsymbol{\varepsilon}_d = \boldsymbol{\varepsilon} - \left(\frac{1}{3} \Delta \right) \mathbf{I}$$

Example

MathCAD

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